

TA**m**MEP Assessment: ICARTT C₂H₆ Measurements

1. Introduction

Here we provide the assessment for the ethane (C₂H₆) measurements during the summer 2004 ICARTT field campaign [Fehsenfeld *et al.*, 2006, Singh *et al.*, 2006]. This assessment is based upon the four wing-tip-to-wing-tip intercomparison flights conducted during the field campaign. Recommendations provided here offer TAbMEP assessed biases for each of the measurements and a systematic approach to unifying the ICARTT C₂H₆ data for any integrated analysis. These recommendations are directly derived from the instrument performance demonstrated during the ICARTT measurement comparison exercises and are not to be extrapolated beyond this campaign.

2. ICARTT C₂H₆ Measurements

Three whole air sampler instruments were deployed on three aircraft. Table 1 summarizes these techniques and gives references for more information.

Table 1. C₂H₆ measurements deployed on aircraft during ICARTT

Aircraft	Instrument	Reference
NASA DC-8	Whole Air Sampler (WAS)	<i>Colman et al.</i> [2001]
NOAA WP-3D	Whole Air Sampler (WAS)	Contact PI: eatlas@rsmas.miami.edu
FAAM BAe-146	Whole Air Sampler (WAS)	<i>Hopkins et al.</i> [2003]

3. Summary of Results

Table 2 summarizes the assessed biases as well as PI reported uncertainties for each of the three C₂H₆ measurements involved in the intercomparisons. More detailed descriptions are provided to illustrate the process for the bias assessment in Section 4.1. The TAbMEP-prescribed IEIP procedures cannot be applied to the ICARTT C₂H₆ measurements for precision assessment. This is because the reported data have large time gaps and a small data population (see Section 3.1 of the introduction). The assessed bias reported in Table 2 (see Section 4.1 for details) can be applied to maximize the consistency between the data sets, by subtracting the value from the reported data to ‘unify’ the data sets. If one assumes instrument performance remained constant throughout the mission, the assessed bias may be extrapolated to the entire mission although it is derived from intercomparison periods only.

Table 2. Recommended ICARTT C₂H₆ measurement treatment

Aircraft/Instrument	Reported 2σ Uncertainty	Assessed Bias (pptv)
NASA DC-8 WAS	10%	-14.92 - 0.0521 C ₂ H ₆ DC-8
NOAA WP-3D WAS	5%	47.75 - 0.0725 C ₂ H ₆ WP-3D
FAAM BAe-146 WAS	Point by Point, average: 5.4% ^a	-49.15 + 0.190 C ₂ H ₆ BAe-146

^a The average encompasses only the comparison period for DC-8/BAe-146.

Figures 1 a and b display the PI reported uncertainties and recommended biases for the three ethane instruments.

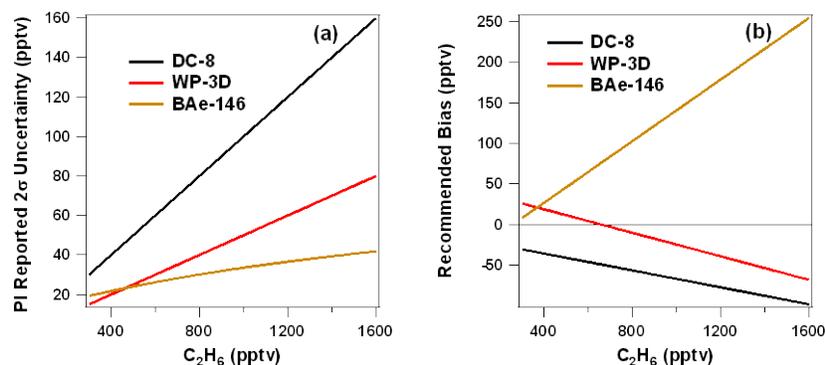


Figure 1. PI reported 2σ uncertainty (panel a) and recommended bias (panel b) for DC-8 (black), WP-3D (red), and BAe-146 (gold) as a function of C₂H₆ level. Values were calculated based upon data shown in Table 2. The BAe-146 PI reported uncertainty was calculated using a function derived from the 60 second merge file.

4. Results and Discussion

4.1 Bias Analysis

Section 3.3 in the introduction describes the process used to determine the best estimate bias. Figures 2 and 4 show the time series plots for the DC-8/WP-3D and DC-8/BAe-146 comparisons. The DC-8 is consistently lower than both WP-3D and BAe-146 by 45 pptv and 67 pptv on average respectively. Figures 5 and 6 show the magnitude of the bias for each intercomparison and Figures 7 and 8 show the corresponding relative residuals.

For 2 of the 3 DC-8/WP-3D flights, there are only 3 or 4 overlapping points with a small range of variation (about 20-40 pptv). It is not statistically significant to show the linear regression for these flights. Therefore, linear regression is performed over the data combined from all three DC-8/WP-3D flights shown in Figure 3. The linear relationships listed in Table 3 were derived from the regression equations found in Figures 3 and 4. The reference standard for comparison (RSC), as defined in the introduction, is constructed by averaging the NOAA WP-3D and NASA DC-8 measurements with equal weights of two each and the FAAM BAe-146 with a weight of one. (i.e. $[2\text{DC-8} + 2\text{WP-3D} + \text{BAe-146}]/5$) The resulting RSC can be expressed as a function of the DC-8 C₂H₆ measurements as the following:

$$\text{RSC}_{\text{C}_2\text{H}_6} = 14.921 + 1.052 \text{ C}_2\text{H}_{6\text{-DC8}}$$

The RSC is then used to calculate the best estimate bias as described in Section 3.3 of the introduction. It should be noted that the initial choice of the reference instrument (DC-8 WAS) is arbitrary, and has no impact on the final recommendations. Table 3 summarizes the assessed measurement bias for each of the three ICARTT C₂H₆ measurements. Note that additional decimal places were carried in the calculations to ensure better precision. It is also noted that the intercept in the equations listed in Table 3 should not be viewed as an offset. These linear equations are used to best describe the linear relation between the measurements.

The WAS technique for measuring VOCs presents some challenges in analyzing the data. The DC-8 data have an integration time of approximately 60-70 seconds, while the WP-3D data have an integration time between 6-11 seconds. For these measurements to be considered simultaneous and correlated, the start and stop times of the WP-3D data must fall within the start

and stop times of the DC-8 data. In order to maximize the data coverage for statistical analysis, one exception is made to this rule. If the shorter (WP-3D) integration time falls outside the longer integration time by no more than two seconds, the data points are also considered to be simultaneous. BAe-146 integration times range from approximately 30-60 seconds. Since the DC-8 and BAe-146 have similar integration times, the measurements are considered correlated if the midpoint of DC-8 or BAe-146 fall within the start and stop time of the other measurement. Only the PI reported data are used in this assessment, and no interpolation is included. It is noted here the integration time difference may potentially be another factor leading to the difference between measurements.

Table 3. ICARTT C₂H₆ bias estimates

Aircraft/ Instrument	Linear Relationships	Best Estimate Bias (a + b C₂H₆) (pptv)
NASA DC-8 WAS	$C_2H_6_{DC-8} = 0.00 + 1.000 C_2H_6_{DC-8}$	$-14.92 - 0.0521 C_2H_6_{DC-8}$
NOAA WP-3D WAS	$C_2H_6_{WP-3D} = 58.43 + 0.981 C_2H_6_{DC-8}$	$47.75 - 0.0725 C_2H_6_{WP-3D}$
FAAM BAe-146 WAS	$C_2H_6_{BAe-146} = -42.26 + 1.3 C_2H_6_{DC-8}$	$-49.15 + 0.190 C_2H_6_{BAe-146}$

As a part of ICARTT intercomparison standard exchange exercises, University of California, Irvine (UCI) prepared the common VOC samples that were sent to University of Miami (Miami), University of New Hampshire (UNH), and University of York (York) for their lab analyses. Some of these same institutions had instruments on the following planes during ICARTT: UCI on the DC-8, Miami on the WP-3D, and York on the BAe-146. The comparison incorporated 9 species, which included ethane. We believe that the inclusion of this comparison result will help the readers better understand the airborne intercomparison analysis. The difference in this lab comparison between the DC-8 and WP-3D instruments was 35 pptv, WP-3D being higher, at a DC-8 instrument reading of 1183 pptv. From the same lab comparison, the difference between the DC-8 and BAe-146 was 67 pptv, BAe-146 being higher. Comparing the ICARTT flights to this lab comparison shows fairly similar results. The difference for the DC-8/WP-3D flights is 10 pptv higher, whereas the difference for the DC-8/BAe-146 flights is the same as the lab comparison. Since instrument performance can vary depending on calibration and environmental factors, and the time intervals were not the same for all instruments, this difference between intercomparisons does not seem unnaturally large.

4.2 Precision Analysis

A detailed description of the precision assessment is given in Section 3.1 of the introduction. The IEIP precision, expected variability, and adjusted precision could not be calculated for C₂H₆ because of the small number of points and large time gaps between measurements.

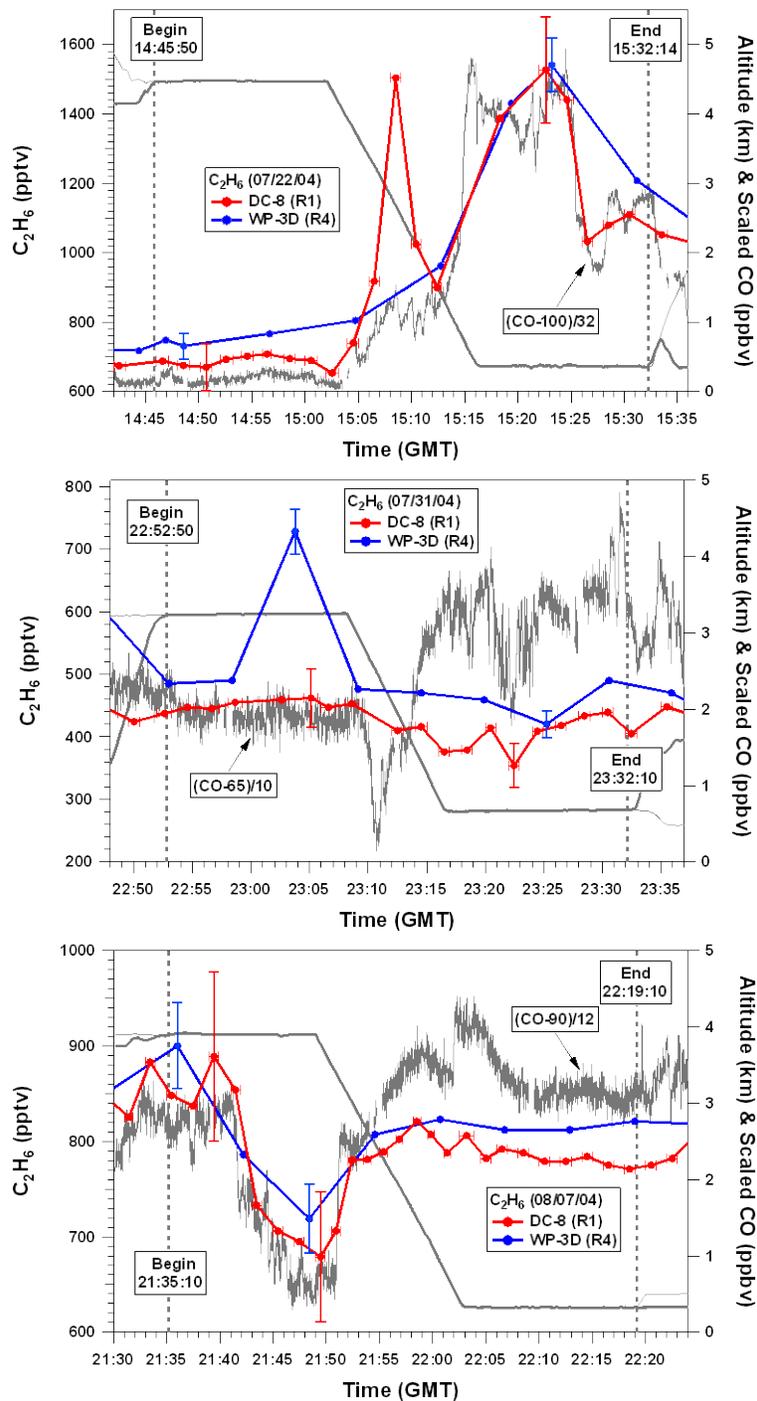


Figure 2. Time series of C_2H_6 measurements and aircraft altitudes from two aircraft on the three intercomparison flights between the NASA DC-8 and the NOAA WP-3D. Error bars represent the PI reported uncertainty. In parenthesis next to the plane is the data version number.

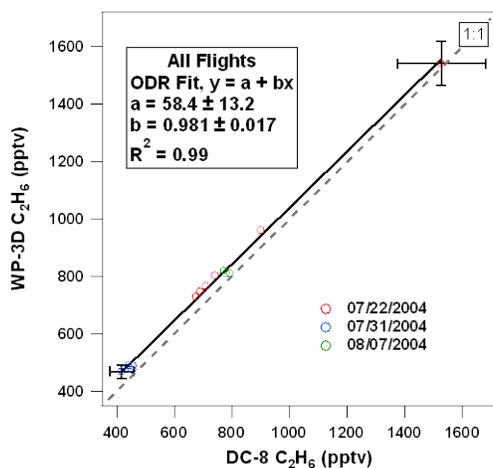


Figure 3. Combined correlation for the C_2H_6 measurements on NASA DC-8 and the NOAA WP-3D for 7/22, 7/31, and 8/07 2004. Error bars represent the PI reported uncertainty.

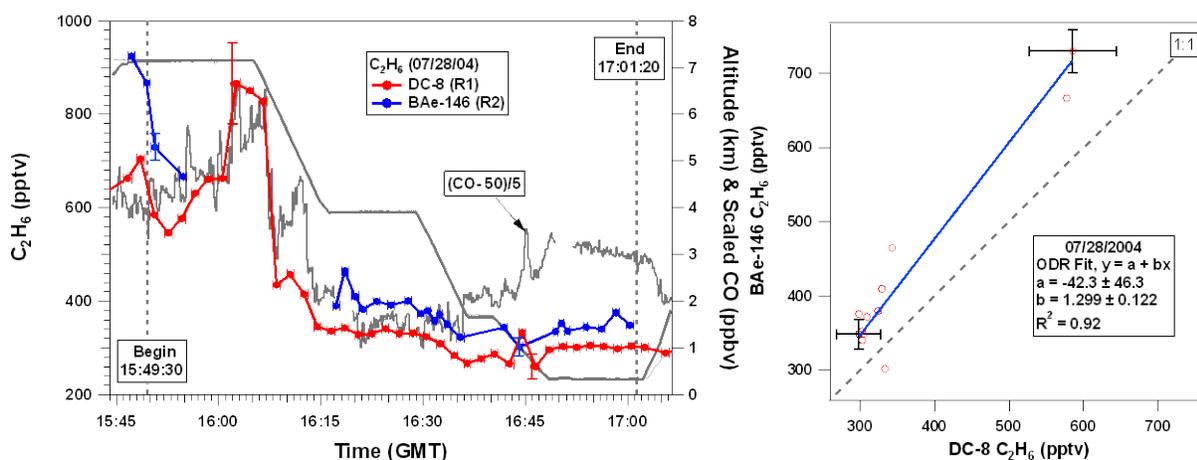


Figure 4. (left panel) Time series of C_2H_6 measurements and aircraft altitudes from the intercomparison flight between the NASA DC-8 and the FAAM BAe-146. In parenthesis next to the plane is the data version number. (right panel) Correlation between the C_2H_6 measurements on the two aircraft. Error bars represent the PI reported uncertainty.

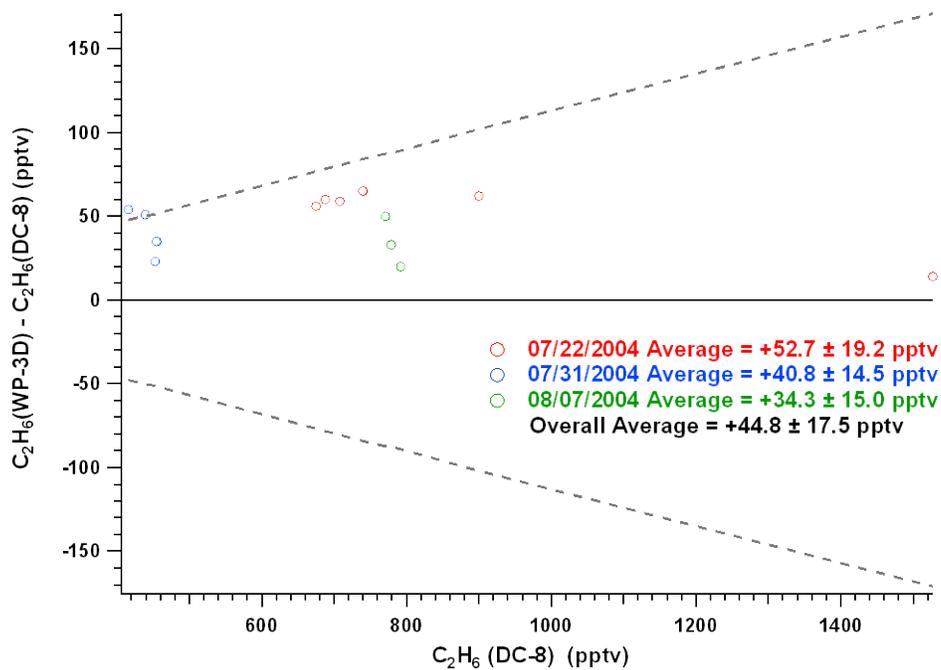


Figure 5. Difference between C_2H_6 measurements from the three DC-8/WP-3D intercomparison flights as a function of the DC-8 C_2H_6 . The dashed lines indicate the range of the results expected from the reported measurement uncertainties.

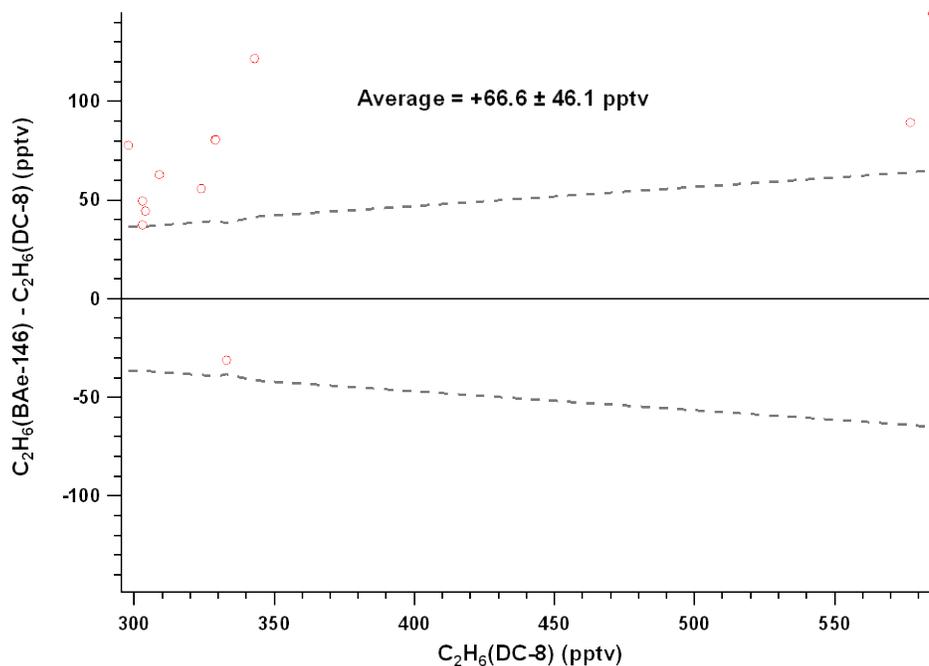


Figure 6. Difference between C_2H_6 measurements from the DC-8/BAe-146 intercomparison flight as a function of the DC-8 C_2H_6 . The dashed lines indicate the range of the results expected from the reported measurement uncertainties.

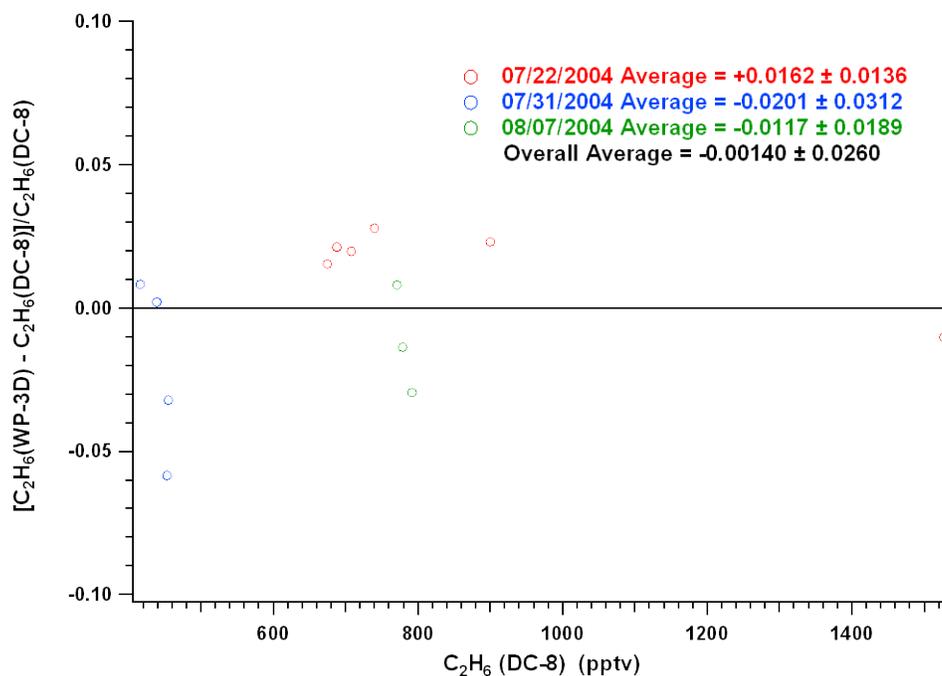


Figure 7. Relative difference between C_2H_6 measurements from the three DC-8/WP-3D intercomparison flights as a function of DC-8 C_2H_6 . A correction was made to account for bias.

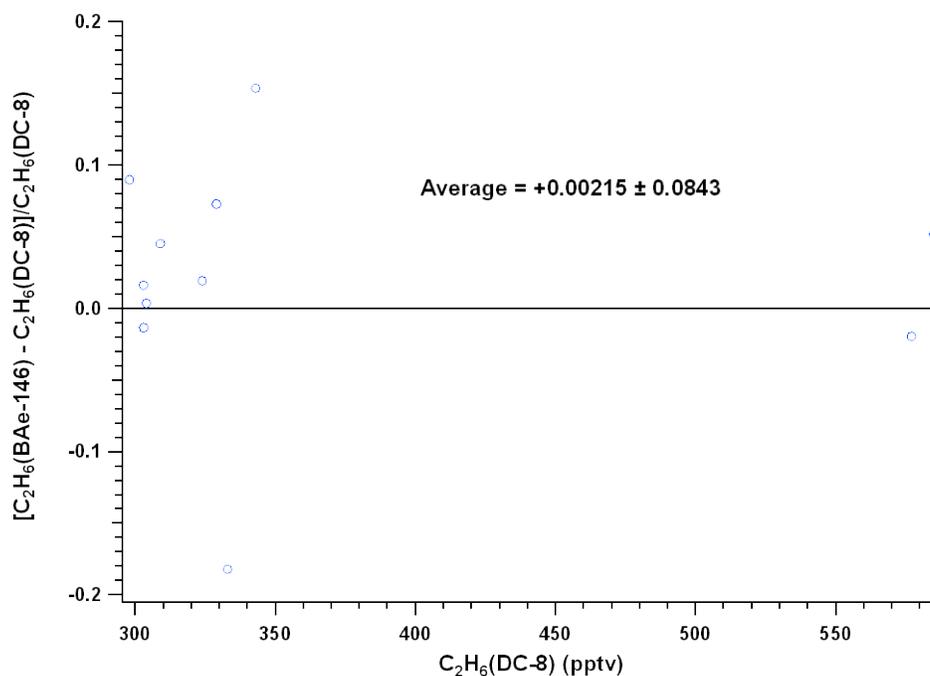


Figure 8. Relative difference between C_2H_6 measurements from the DC-8/BAe-146 intercomparison flight as a function of DC-8 C_2H_6 . A correction was made to account for bias.

References

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